

(19) World Intellectual Property Organization
International Bureau



(43) International Publication Date
28 March 2002 (28.03.2002)

PCT

(10) International Publication Number
WO 02/24597 A2

(51) International Patent Classification⁷: **C04B 28/26**

(21) International Application Number: PCT/US01/29376

(22) International Filing Date:
18 September 2001 (18.09.2001)

(25) Filing Language: English

(26) Publication Language: English

(30) Priority Data:
60/233,952 20 September 2000 (20.09.2000) US
09/871,765 1 June 2001 (01.06.2001) US

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(81) Designated States (*national*): AE, AG, AL, AM, AT, AU,
AZ, BA, BB, BG, BR, BY, BZ, CA, CH, CN, CO, CR, CU,
CZ, DE, DK, DM, DZ, EC, EE, ES, FI, GB, GD, GE, GH,
GM, HR, HU, ID, IL, IN, IS, JP, KE, KG, KP, KR, KZ, LC,
LK, LR, LS, LT, LU, LV, MA, MD, MG, MK, MN, MW,
MX, MZ, NO, NZ, PH, PL, PT, RO, RU, SD, SE, SG, SI,
SK, SL, TJ, TM, TR, TT, TZ, UA, UG, UZ, VN, YU, ZA,
ZW.

(84) Designated States (*regional*): ARIPO patent (GH, GM,
KE, LS, MW, MZ, SD, SL, SZ, TZ, UG, ZW), Eurasian
patent (AM, AZ, BY, KG, KZ, MD, RU, TJ, TM), European
patent (AT, BE, CH, CY, DE, DK, ES, FI, FR, GB, GR, IE,
IT, LU, MC, NL, PT, SE, TR), OAPI patent (BF, BJ, CF,
CG, CI, CM, GA, GN, GQ, GW, ML, MR, NE, SN, TD,
TG).

Published:

— *without international search report and to be republished
upon receipt of that report*

*For two-letter codes and other abbreviations, refer to the "Guid-
ance Notes on Codes and Abbreviations" appearing at the begin-
ning of each regular issue of the PCT Gazette.*

(54) Title: **INORGANIC MATRIX COMPOSITIONS, COMPOSITES AND PROCESS OF MAKING THE SAME**

(57) **Abstract:** A modified alkali silicate composition for forming an inorganic network is made by reacting an alkali silicate (or precursors such as an alkali hydroxide, a SiO₂ source and water), an acidic oxoanionic compound such as phosphoric acid, water and optionally one or more multivalent cation(s) selected from Groups 2, 3, 4, 5, 6, 11, 12, 13, 14, 15 or 16 of the periodic table such as an alkaline earth salt, water and optional processing aids. A composite can be prepared by applying the modified aqueous alkali silicate composition to a reinforcing medium and curing the composite at a temperature from 15°C up to 1000°C and a pressure of up to 20,000 psi (137.895 MPa). Composite and neat resin components prepared from the invention can exhibit excellent dimensional stability to 1000°C and higher, and can be prepared at temperatures and pressures typical for organic polymer processing. The composite can be shaped by compression molding as well as other known fabrication methods.

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INORGANIC MATRIX COMPOSITIONS, COMPOSITES AND PROCESS OF MAKING THE SAME

Background of the Invention

5 The present invention relates to thermally resistant inorganic matrix compositions incorporating a silicate network, which can be processed within a wide range of temperatures and pressures. Whereas the physical and thermal properties of the inorganic matrix binder as well as composites may be enhanced utilizing elevated processing temperatures, exceptional composite and neat resin components can be prepared at lower processing conditions which are
10 not typical for ceramic composites, but which are comparable to those used for typical high-performance organic polymer processing (temperatures 15°C to 200°C and pressures <200 psi or 1.378 MPa). The composite materials formed at the lower processing conditions exhibit excellent thermal, dimensional, physical and flameproof properties.

 Inorganic matrix compositions of the present invention are useful as fire retardant
15 binders, bulk materials, adhesives or composite materials. As bulk materials, they are used to form shaped objects which when cured provide a structural material. As a composite material, the matrix composition is used to impregnate a fabric, which may be combined with other similarly impregnated fabrics to form a lay-up, which in turn is then shaped and cured to form a shaped composite or object, similar to a bulk material, but with the benefit of the reinforcement
20 provided by the fabric.

 The basic concept of composite materials has been known for centuries. Composite materials offer a unique blend of value added features, such as weight savings, electrical insulation, thermal insulation, corrosion resistance, and manufacturing cost savings. These features in some instances can overshadow the material cost in specialized applications ranging,
25 for example, from advanced sporting equipment to the F-22 aircraft fuselage. However, current state-of-the-art composite materials can also exhibit properties that present serious barriers to entry in some high-performance markets. These include poor flame, smoke and toxicity (FST) performance, physical degradation at high temperatures as well as higher material and processing costs. When exposed to fire or high temperatures (>500°C), conventional composite materials
30 can combust and generate toxic smoke and/or gases. The exceptions, such as ceramic matrix composites and metal matrix composites, are too expensive (often more than \$500/lb) to gain a significant market presence. Clearly, a market need exists for affordable high temperature-resistant, insulating structures.

The most familiar composite systems today are based on organic polymer matrices such as epoxy/glass fiber, epoxy/carbon fiber, polyurethane/glass fiber, PVC/glass fiber, polyimide/quartz fiber, polyester/glass fiber and nylon/glass fiber. Although organic polymer composites exhibit excellent physical and mechanical properties, they are limited with regard to flammability, smoke and gas generation and elevated service temperatures. The flammability of organic polymer-based composites can be reduced by the addition of inorganic components and/or additives. The substitution of hydrogen atoms with halogen atoms (e.g. chlorine) in hydrocarbons and hydrocarbon polymers can significantly reduce flammability and smoke/gas generation but will degrade at high temperatures ($>250^{\circ}\text{C}$) and eventually incinerate at higher temperatures ($>450^{\circ}\text{C}$). Organic thermoplastic polymers also deform at relatively low temperatures (100°C to 300°C) and organic polymers designed for higher service temperatures are generally prohibitive in material and processing costs.

Composite materials offer a unique blend of value added features, such as weight savings, electrical insulation, thermal insulation, corrosion resistance, and manufacturing cost savings. These features in some instances can overshadow the material cost in specialized applications ranging, for example, from automotive fascia to the F-22 aircraft fuselage. However, current state-of-the-art composite materials can also exhibit performance characteristics that present serious barriers to entry in some high-performance markets. These include poor flame, smoke and toxicity (FST) performance, physical degradation at high temperature as well as higher material and processing costs. When exposed to fire or high temperatures (above 500°C), conventional composite materials combust and can generate toxic smoke. The exceptions, such as ceramic matrix composites and metal matrix composites, are too expensive (often more than $\$500/\text{lb}$) to gain a significant market presence. Affordable high temperature-resistant, insulating structures have potential applications which minimize fire and heat transfer damage to sensitive areas, aircraft carrier blast or heat shields, high-temperature thermal insulation for wiring or other sensitive components susceptible to thermal damage, piston insulators, high temperature insulating structures, and fire barriers.

Composite matrices frequently are based on organic polymers such as epoxy, polyimide, polyamide, polyester and other resins. Other composite materials include metal matrix composites (MMC), ceramic matrix composites (CMC), carbon-carbon composites as well as other inorganic matrix composites. A composite matrix may be 100% inorganic, or it may contain some organic content. Inorganic matrix networks include ceramics, silicates, glasses,

aluminum silicates, alkali aluminum silicates, potassium silicates, sodium silicates, silicon carbides, silicon nitrides, alumina, cementitious materials, metals, metal alloys or other matrix materials known to those knowledgeable in the arts. Other materials that can be considered include inorganic particles encapsulated with inorganic binders, organic resins filled with inorganic fillers, inorganic-organic hybrids such as silicone, and other inorganic matrix materials known to those knowledgeable in the arts.

Alkali silicates are employed as affordable inorganic matrix binder materials. See for example, US Patent numbers 4,472,199; 4,509,985; 4,888,311; 5,288,321; 5,352,427; 5,539,140; or 5,798,307 to Davidovits; US Patent number 4,936,939 to Woolum; or US Patent number 4,284,664 to Rauch. However, alkali silicates possess a high pH, which can frequently damage glass fibers by both chemical and physical means, severely degrading its strength. Furthermore, the cured composites taught by these patents still exhibit a high pH in a solid form, which continues to promote glass fiber degradation. So, the physical performance of a fiberglass/alkali silicate composite usually is extremely poor. This has been compensated by reinforcing the alkali silicate matrix with carbon fiber reinforcements rather than fiberglass. This replacement suffers in comparison to a composite prepared with fiberglass reinforcement in several respects such as material cost since carbon fibers are several times more expensive than glass fibers. Carbon fibers are also electrically and thermally conductive, which eliminates many important dielectric and thermal insulating applications and carbon fibers severely oxidize at 450°C, which eliminates many important high temperature applications. Also, when carbon fibers are combined with the alkali silicate matrix they have two different thermal expansion coefficients, which can lead to microcracking during thermal cycling.

Furthermore, cured alkali silicates (including alkali aluminum silicates) are also caustic when exposed to moisture, yielding a caustic solution, which is undesirable. Caustic by-products may accelerate corrosion in adjacent materials, in many applications, and the extreme caustic nature of the cured material suggests hydrolytic instability. Improved inorganic matrix materials that are less caustic may enable a much broader range of applications.

Summary of the Invention

The present invention is the result of the discovery that an inorganic silicate polymer network can be achieved using a composition which is simply a modified alkali silicate. The modified alkali silicate network of the present invention can be prepared either of two ways: (1) As the reaction product of an alkali silicate, an acidic network former (an acidic oxoanionic

compound such as phosphoric acid), water and optionally a clay filler, and one or more network modifiers (a multivalent cation(s) selected from Groups 2, 3, 4, 5, 6, 11, 12, 13, 14, 15 or 16 such as an alkaline earth salt) or (2) as the reaction product of an alkali hydroxide or oxide, a silica source and water as well as the acidic network formers and network modifiers. The ability to vary these "building blocks" enables one to tailor product properties to suit numerous high-temperature applications. The composition can incorporate other network forming materials, modifiers and fillers.

Alkali silicate based composites can be prepared by applying an aqueous slurry of the modified alkali silicate matrix precursor to a reinforcing medium, such as a continuous or discontinuous glass or carbon fiber mat. After an optional B-staging period the composite is cured within a temperature range of 15°C to 1000°C and higher, and at a pressure sufficient to consolidate the composite, usually at an external pressure range from ambient to 20,000 psi (137.895 MPa) and under a vacuum of ambient to 10^{-3} torr (e.g., vacuum bagging). The preferred range for the temperature is between 50°C to 200°C and at a pressure of less than 200 psi (1.378 MPa) with or without vacuum bagging. The term "B-staging" is a common term used in composite technology to describe the practice of allowing a polymer matrix precursor to react and proceed to a partially polymerized intermediate stage short of a fully cured polymer network. Vacuum bagging can also be implemented to aid water removal and consolidation. Compression molding, as well as other typical molding methods, can be used to shape the composite as desired.

The resulting neat resin and/or composite exhibits dimensional stability up to 1000°C and higher, depending upon the formulation and processing and possesses excellent properties with respect to flame, smoke and toxicity. Furthermore, a composite made using the inorganic polymer network forming composition of the present invention is lightweight with good thermal and electrical insulating characteristics. Various shapes are relatively inexpensive to manufacture primarily due to the low temperature and pressures needed to effect cure of the composite.

The composition is also useful as an adhesive composition, a coating, a neat resin, sheet molding compound or as a bulk molding compound. The compositions of the present invention are useful in those applications where good thermal and physical stability are desired, such as those applications for which ceramic composites are used.

Detailed Description of the Invention

The inorganic polymer network of the present invention is prepared by reacting an alkali silicate solution, an acidic oxoanionic compound such as phosphoric acid, water, and optionally, one or more multivalent cation(s) selected from Groups 2, 3, 4, 5, 6, 11, 12, 13, 14, 15 or 16 of the Periodic Table such an alkaline earth salt and optionally a clay filler. Alternately, the reaction of a silica source, an alkali base, water, an acidic oxoanionic network former, and optionally, one or more cationic network modifier(s) and/or a clay filler, can yield a high-temperature inorganic polymer network. Additional components such as fillers, other network forming materials and modifiers can be incorporated as needed. These include traditional fillers such as kaolin, metakaolin, montmorillonites mica and other clay or mineral fillers. Modifiers can include crosslinkers and gel inhibitors/promoters such as mineral acids, organic acids and bases. The modified alkali silicate composition that is obtained can be cured at relatively low temperatures ($<200^{\circ}\text{C}$), and at low pressures (<200 psi or 1.378 MPa) to produce a inorganic polymer network having dimensional and thermal stability to 1000°C and higher. That is, a structure incorporating the matrix composition of the present invention exhibits no substantial permanent dimensional change (i.e., less than one percent) at temperatures to 700°C and higher. However, it is not restricted to the lower temperature or pressure, and if needed, or desired, properties can be further enhanced utilizing elevated processing temperatures (up to 1000°C and higher) and pressures (up to 20,000 psi (137.895 MPa)), or incorporating post-cure heat treatments.

The alkali silicates utilized can include a wide range of silica/alkali oxide ($\text{SiO}_2/\text{A}_2\text{O}$) ratios and % solids levels. Such solutions can be purchased from commercial sources or prepared immediately prior to use from precursors such as a silica source and an alkali hydroxide, alkali oxide, carbonate or combination thereof. The alkali silicate can be derived from an alkali base, such as potassium hydroxide or sodium hydroxide, from potash or soda ash and a silica source. The SiO_2 source can be an amorphous or crystalline SiO_2 form, such as silica, silica fume, precipitated silica, microsilica, sand, microcrystalline silica, silica gels, colloidal silica, quartz, quartz flour, a sodium silicate solution, a potassium silicate solution as well as solid sodium and/or potassium silicates.

The thermal and physical properties of the inorganic matrix binder can be influenced by the nature of the silica source, for example, the incorporation of a dense crystalline α -quartz network can enhance dimensional stability while, in turn, introducing an open, amorphous silica

source will produce a lower density network. Also, some sources of silica fume contain traces of carbon that can lead to discoloration in the final product. When the alkali silicate is derived from an alkali hydroxide and a silica source, the alkali hydroxide is present in an amount of 3 wt. % to 25 wt. % based upon the weight of the total composition or mixture, preferably 7 wt. % to 15 wt. %.

5 %. The silica source is present in an amount of 10 wt. % to 75 wt. %, preferably 15 wt. % to 60 wt. %. The total mixture, in this instance, includes an alkali hydroxide, a silica source, phosphoric acid, an alkaline earth salt, a clay filler and water. In some cases, for example, when an alkali silicate solution is used, a portion of the alkali hydroxide, silica and water provided is included in the ranges disclosed.

10 The acidic oxoanionic compound can be boric acid, phosphoric acid, sulfuric acid, nitric acid, sodium dihydrogen phosphate, disodium hydrogen phosphate, potassium hydrogen phosphate, ammonium hydrogen phosphate, or compounds incorporating borate, sulfate, aluminate, vanadate, germanate, and the like ions. The preferred acidic oxoanionic compound is phosphoric acid, H_3PO_4 , which can be used in any grade or concentration although a more

15 concentrated material is preferred to minimize the water content. The acidic oxoanionic compounds can be used in any combination or in addition to the phosphate compounds. The acidic oxoanionic compound is present in an amount of between 0.01 wt. % and 20 wt. % based upon the total composition. The preferred amount of acidic oxoanionic compound is between 2 wt. % to 5 wt. %.

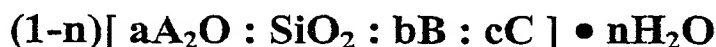
20 The multivalent cations which are selected from Groups 2, 3, 4, 5, 11, 12, 13, 14, 15 and 16 of the Periodic Table are used in an amount of between zero and 20 wt.% based upon the total mixture, and if included, the ranges of 1.0 wt. % to 5 wt. % is further preferred. The multivalent cation containing compounds can comprise any alkaline earth metal salt, including nitrates, sulfates, and chlorides, although magnesium nitrate, $\text{Mg}(\text{NO}_3)_2$ is the preferred alkaline earth

25 salt. Other compounds such as $\text{Zn}(\text{NO}_3)_2$ can be incorporated to modify network density. Other network modifiers can include compounds incorporating boron, aluminum, lead, zinc, gallium, cadmium, titanium, zirconium, lanthanum, cerium, neodymium, yttrium, calcium, strontium, barium, lithium, rubidium, cesium, and fluorine.

30 The clay filler is preferably calcined kaolin and is used in an amount from none to 25 wt. % based upon the weight of the total composition, with 3 wt. % to 5 wt. % being further preferred. The calcined kaolin may prove to be reactive with the silicate matrix material, although reactivity of the clay filler is not required and any of the commercially available clay fillers can be employed.

The balance of the uncured composition is water and it will comprise 10 wt. % to 70 wt. % based upon the total composition weight. The range of 15 wt. % to 40 wt. % is further preferred. The water can be introduced as part of one of the components, such as part of an alkali silicate solution, an alkaline earth salt solution or part of a phosphoric acid solution. Since the water incorporated in this invention can be viewed as a reaction medium, a reactant as well as a reaction product, the concentration of water can be difficult to quantify in general. The initial level of water in the starting mixture can vary from 10 wt. % to 70 wt. % while a B-staged prepreg may contain 5 wt. % to 35 wt. % water. A cured sample of the inorganic binder and/or composite can contain zero to 10 wt. % water depending upon the processing conditions.

The starting chemical composition of the invention (excluding fillers), which is derived from the aqueous mixture or slurry, can be described by the following formula which is a qualitative representation of the starting materials:



Where:

$A = [(1-z) K_2O, (z)Na_2O]$, where z ranges from 0 to 1.

K_2O is potassium oxide.

SiO_2 is silica, derived from a silica source such as Kasil-1, silica fume, silica, silica gel or a combination thereof.

H_2O is water.

a = preferred molar ratio of $A_2O : SiO_2$, which ranges from 1.00 to 0.05.

b = preferred molar ratio of $B : SiO_2$, which ranges from 0.500 to 0.001.

c = preferred molar ratio of $C : SiO_2$, which ranges from 0.250 to 0.000.

n = molar ratio of H_2O incorporated into the formulation.

During initial formulation, the desired range is from 0.1 to 0.9, where $n = 0.2$ to 0.4 is the preferred embodiment.

After cure, n is less than 0.25, where $n < 0.1$ is the preferred embodiment.

B = additional network former(s), such as P_2O_5 , SO_3 , etc., derived from an acidic precursor, such as H_3PO_4 , H_2SO_4 , etc., or a combination thereof.

C = optional secondary network linking unit(s) such as Mg^{2+} , Zn^{2+} , Ti^{4+} derived from multivalent main group metal and/or transition metal compounds such as $Mg(NO_3)_2$, $Zn(NO_3)_2$, etc., or a combination thereof.

The ability to vary these "building blocks" enables one to tailor product properties to suit numerous high-temperature applications. The composition can incorporate other network forming materials, modifiers and fillers.

The reinforcing medium can be a material composed of reinforcing fibers, such as continuous or discontinuous fibers, which will be encapsulated in the matrix material. Reinforcing fibers may include glass fibers, carbon fibers, graphite fibers, mineral fibers, metallic fibers, quartz fibers, ceramic fibers, silicon carbide fibers, stainless steel fibers, titanium fibers, nickel alloy fibers, polymeric fibers, aramid fibers, basalt fibers, alkaline resistant glass fibers and/or other fibers known to those knowledgeable in the arts. Reinforcing fibers may be in many forms, including yarns, tows, whiskers, continuous fibers, short fibers, woven fabrics, knitted fabrics, non-woven fabrics, random mats, felts, braided fabrics, wound tows, and/or other forms known to those knowledgeable in the arts.

The matrix compositions may incorporate a wide variety of organic and inorganic fillers commonly used by those knowledgeable in the art. The matrix may incorporate filler materials such as ceramic powders, mineral powders, silicon carbides, silicon nitrides, silicates, aluminum silicates, sodium aluminum silicates, potassium aluminum silicates, carbon, carbon black, molybdenum and its compounds, or other fillers known to those knowledgeable in the arts. Organic materials are less preferred where the application is such that the organic materials will combust and produce gases. The filler materials also could be spheres or particles, such as microspheres, macrospheres, hollow spheres, and solid spheres.

The matrix composite material system of the present invention influences the pH of the solution containing the alkali silicate backbone by incorporating an acidic inorganic component (such as a protonated oxoanions such as phosphoric or boric acid) and acidic salt modifier such as an alkaline earth salt. The alkali silicate solutions require a high pH to maintain a high concentration of monomeric silicate anions needed to moderate network formation. The ability to cure under moderate conditions after reducing the pH to a lesser value reduces the damage to the glass fiber reinforcement induced by the alkalinity of the matrix. The inorganic matrix binder cures via a condensation reaction partially driven by the elimination of water from the framework and excessive water in the binder leads to a lack of dimensional stability, poor physical properties and difficulty in processing.

The composite material can be prepared using any of the composite molding methods typically employed, the test specimen for this example was formed into cross-ply multi-layer composite by a traditional prepreg/layup method. A "prepreg" is formed by impregnating a

reinforcing medium or reinforcement with the matrix binder to produce a binder coated fabric sheet. The next step is to layer the individual prepregs together to achieve the desired thickness and/or shape. Next, the "layup" is placed into a mold to compact or consolidate the prepregs and to form the composite shape. Optionally, the prepregs could be subjected to a B-staging period and/or vacuum bagging to reduce the water content. Finally, the composite is cured within a temperature range of 15°C to 1000°C and higher, and a pressure range from 0 psi to 20,000 psi (137.895 MPa), preferably at a temperature between 50°C to 200°C and at a pressure less than 200 psi or 1.378 MPa.

As can be appreciated, the matrix composites of the present invention can be fabricated and processed using compression molding, bulk molding compound, sheet molding compound, powder and reinforcement, liquid and reinforcement, prepreg and sintering. Additional methods include pultrusion (an automated process capable of producing a constant cross-section product), wet lay-up (a simple manual process for rapid prototypes and affordable low performance products), filament winding (an automated process for bodies of revolution), vacuum bag processing (a typical process for high performance aerospace laminates), autoclave or non-autoclave, vacuum infusion (a process for large thick high-performance parts), liquid resin, film infusion or powder infusion, resin transfer molding (a near net-shape molding process with excellent dimensional repeatability), extrusion (a process capable of producing constant cross-section non-structural short-fiber products), injection molding (an automated process capable of producing small non-structural short-fiber products), casting (a process for bulk non-structural products), spin casting (a process capable of producing high-quality tubing), trapped elastomer molding (a process capable of producing unusual shapes), and like processes.

These processes have several advantages compared to the curing/consolidation methods normally used in making high temperature inorganic polymers, namely ceramics and glasses. Ceramic and glass processing typically requires high temperature processing equipment (above 1000°C). The nature of the inorganic matrix formulation of the present invention allows composites to be processed with conventional equipment found in thousands of composites manufacturing facilities. These processes allow a more rapid throughput than typical ceramic processes and enables the easy manufacturing of larger parts than typical ceramic processes. The use of these processes allows high fiber volumes for structural integrity, which is superior to typical concrete processing.

Glass fiber reinforcement (including E-glass fibers, S-glass fibers, alkali resistant glass fibers, etc.) is the preferred reinforcing material and it allows several unique performance features. The composite materials using glass fiber reinforcement and the matrix binder of the present invention are affordable, non-combustible, thermally-stable [i.e., no measurable (<0.2%) permanent dimensional change after 48 hours of exposure at 700°C] composite materials with insulating qualities and structural qualities that can be processed at lower temperatures using typical processing equipment. Normal processing can be at relatively low temperatures (<200°C) and low pressure (<200 psi or 1.378 MPa). A cross-ply glass fiber laminate can be produced with thermal insulating qualities (e.g., thermal conductivity of nominally 1.4 W/m-K), electrical insulating qualities (no detectable electrical conductivity when measured with a standard ohm meter) and modest mechanical performance (flexural modulus up to 8 Msi, flexural strength to 20+ ksi, and ultimate flexural strains up to 1.3%). This combination of properties should be enabling technology for many applications.

Ceramic fiber reinforcement (including silicon carbide fibers) is another preferred reinforcement, especially for high temperature applications above 700°C. Although expensive, ceramic fibers maintain structural integrity well above 1000°C. Carbon fiber reinforcement is a preferred reinforcement where electrical conductivity, thermal conductivity, high strength and/or impact resistance is desired.

The following material properties and standardized tests are used to evaluate the performance of composites prepared with the inorganic matrix binders of the present invention: hydrolytic stability; flexural strength (ASTM D790-99), flexural modulus (ASTM D790-99), ultimate flexural strain (ASTM D790-99), specific gravity (ASTM D792), thermal dimensional stability, thermal conductivity (modified ASTM C177), electrical conductivity; pH (of the resin solution, the neat resin and the composite structure) Differential Scanning Calorimetry (or DSC); combustibility, thermal conductivity (ASTM C177), electrical conductivity (ASTM D 257), voltage breakdown (ASTM D229), permittivity @ 1 MHz (ASTM D229), dissipation factor @ 1 MHz (ASTM D229), arc resistance (ASTM D229), Izod impact strength (lengthwise & crosswise) (ASTM D229), flammability (UL 94, ASTM E-1354), dielectric constant; temperature index (NEMA LI-6), tensile strength, modulus and ultimate strain (ASTM D 638), compression strength, modulus and ultimate strain (ASTM D 695), interlaminar shear strength (ASTM D3846), short beam shear strength (ASTM D2344) and compression after impact.

The formulations disclosed within the terms of the present invention may also comprise any additives and fillers commonly in usage with regular hydraulic binders.

Furthermore, the use of the matrix binder is not solely limited to composites but can be used to form neat resin components, coatings and adhesives.

5 As can be appreciated, the present invention can be formulated to be non-combustible. This desirable safety feature differentiates the invention from most organic materials (such as plastics, wood, rubber, etc.) that tend to combust, generate smoke and/or toxic gases upon exposure to fire. Further, the present invention can be formulated to be a thermal insulator and/or an electrical insulator. This desirable feature differentiates compositions in accordance with the
10 present invention from most metals (such as steel, aluminum, copper, etc.), that tend to be thermal and electrical conductors.

The present invention can be formulated to perform at high temperatures ($>1000^{\circ}\text{C}$) with negligible permanent changes in dimensions. This desirable feature differentiates the invention from most organic materials (which tend to pyrolyze when exposed to temperatures above
15 500°C), from most cement formulations (which tend to spall above 300°C) and from many metals (including aluminum), that tend to warp or melt at 700°C . As a further feature, the present invention can achieve high temperature performance (above 1000°C) while being processed at relatively low temperatures, ($<200^{\circ}\text{C}$) and low pressures (e.g. $<200^{\circ}\text{C}$ and <200 psi or 1.378 MPa). This feature is desirable because the ability to process at low temperatures and
20 pressures allows the invention to be processed with more affordable equipment and manufacturing processes. This feature of the chemistry differentiates the present invention from most ceramics, glasses and metals, which generally require very high temperatures and/or high pressures to create a molded shape. (Of course, the invention also can be effectively processed at higher temperatures and pressures; we have processed the material above 10,000 psi (68.948
25 MPa) and above 1500°C).

The present invention can be formulated to impregnate fibers to form a rigid composite material. This desirable feature differentiates the invention from most materials, because most rigid materials have not been processed as a low viscosity liquid capable of wetting fibers. Fiber reinforcement within a matrix material offer many benefits, including improved strength,
30 stiffness, fracture toughness, fatigue, strength and impact resistance. While fiber-reinforced composite materials are common in applications ranging from advanced sports equipment to F-22 aircraft structures, the vast majority of composite materials are made with organic matrix materials, which are combustible. Non-combustible composite materials, such as ceramic matrix

composite materials and metal matrix composite materials, tend to be cost prohibitive for most applications because of the high processing temperatures required. The present invention can be processed at much lower cost than most ceramic or metal matrix composite materials. These desirable features differentiate the present invention from many materials, including numerous metals.

These desirable features differentiate the present invention from many materials, including many metals. Given these features, the present invention is suited for many applications, including fire barriers, heat shields, high-temperature insulators, high-temperature molds, friction products, tooling and structures in high temperature environments.

The present invention readily can be formulated to incorporate a wide variety of fillers to tailor the material performance to suit the specific application. These fillers which may include hollow spheres, conductive fillers, friction and/or thermal additives, etc. can be incorporated to modify physical properties including density, conductivity, coefficient of friction, thermal performance, etc.

The following examples are illustrative of the present invention, and should not limit the scope of the invention.

General Example

The following example will serve to illustrate a matrix binder in accordance with the present invention (Ingredients shown in Table 1):

The alkali base, potassium hydroxide (KOH, 26.0 g) is dissolved in water (160.0 g) at room temperature with gentle stirring. An exotherm will occur and the mixture can be cooled as needed, such as refrigerating the mixture to approximately 5°C to minimize any exothermic reaction with the silica fume. The silica fume (90.0 g) is then added to the KOH solution while being stirred with a high-shear mixer. The phosphoric acid solution (12.0 g 85% H₃PO₄ in 12.0g water) is added dropwise to assure that the mixture does not gel. After this addition is completed, calcined kaolin, metakaolin or kaolin powder (15.0 g) is added with high-shear mixing. Finally, the magnesium nitrate solution (2.5 g Mg(NO₃)₂•6H₂O in 2.0 g water) is added, again with vigorous stirring for approximately an additional 10 minutes. The mixture is allowed to set until the viscosity rises to a level (approximately 150 centipoise) suitable for application to the reinforcement medium (fabric, chopped fiber, wound filament, etc.) needed to construct the composite. If a neat sample is required, the amount of water used can be reduced. The

composite material can be prepared using any of the composite molding methods typically employed, the test specimen for this example was formed into a composite by a traditional prepreg/lay-up method. A "prepreg" is formed by impregnating a reinforcing medium or reinforcement with the matrix binder to produce a binder coated fabric sheet. The next step is to layer the individual prepregs together to achieve the desired thickness and/or shape. Next, the "lay-up" is placed into a mold to compact or consolidate the prepregs and to form the composite shape. Optionally, the prepregs could be subjected to a B-staging period and/or vacuum bagging to reduce the water content.

Fiberglass composite panels were made using the matrix binder of Example 1 and compression molded using standard composite processing parameters: curing at 200 psi (or 1.378 MPa) and 80°C for 3 hours, 110°C for 3 hours and 150°C for 3 hours. The fiberglass composite is electrically non-conductive (no detectable conductivity as measured with a standard ohmmeter) and has a thermal conductivity of 1.4 W/m-K, which is similar to plate glass. The cured resin is brittle but exhibits an ultimate flexural strain of 0.5%, as compared to ceramics which typically fail at 0.1% strain. The composite is able to carry a load after being struck with a hammer, while ceramics will shatter. Flame, smoke & toxicity (FST) performance was confirmed by exposure of 2 mm thick specimen to a 1600°C propane flame for 120 seconds during which the panel did not ignite nor produce smoke or fumes. The silicate network is designed for thermal stability and it exhibits no significant permanent dimensional change (<0.2%) after 48 hours of exposure to 700°C.

Examples 1 – 5:

Modified alkali silicate compositions were made in accordance with the process set forth in the General Example, but the ingredients were varied as shown in Table 1.

Table 1: Matrix Formulations in Examples 1 – 5.

Ingredients		Example 1 (g)	Example 2 (g)	Example 3 (g)	Example 4 (g)	Example 5 (g)
H₂O		160.0	72.4	98.3	693.3	---
KOH		26.0	70.5	70.5	649.0	138.4
Silica Source	Kasil-1*	---	---	---	---	244.4
	Silica fume	90.0	206.3	206.3	---	---
	Silica gel	---	---	---	379.6	---
	Quartz flour**	---	---	---	1518.4	423.7
Acidic Oxoanionic Compound	H₃PO₄	12.0	22.9	---	211.0	52.75
	H₂O	12.0	22.9	---	211.0	52.75
Filler	Kaolin	15.0	34.4	34.4	316.0	79.0
Multivalent Cation(s) Compound	Mg(NO₃)₂ • 6 H₂O	2.50	11.45	---	105.0	26.25
	H₂O	2.0	5.75	---	53.0	13.25

* Kasil-1 (Potassium silicate solution, 2.50 SiO₂:K₂O, PQ Corporation, Valley Forge, PA.)

** Tamsil (Microcrystalline Silica from Unimin Specialty Minerals, Inc., Tamm, IL)

Example 6

The aqueous slurry composition of Examples 2 and 3, each having a viscosity of 150 centipoise, were used to impregnate, using a laboratory scale treater, an E-glass fabric 7781, which was taken from a 10 inch (25.4 cm) wide roll of fabric. The roll was cut into sheets and staged at room temperature for 30 minutes. Ten sheets of fabric, which were similarly prepared, were layered on a release-coated surface to give a composite that was approximately 0.110 inch thick (0.2794 cm). This was done with the composition of Example 2 and then repeated with the composition of Example 3 so two different composites were formed. Each composite panel was inserted into a vacuum bag and placed under vacuum of 28.5 inches of mercury (or 0.98138 Kgf/cm²) for 2 hours. The vacuum bagged panels were then inserted into a press between two plates and cured at 80°C for 3 hours under 200 psi (1.378 MPa) pressure and 28.5 inches of mercury (or 0.98138 Kgf/cm²) of vacuum. The pressed panels were removed from the press and post baked at 80°C for 12 hours, 110°C for 12 hours, and 150°C for 4 hours. The results are reported in Table 3.

Table 3: Mechanical Strengths of Composites cured in Examples 6, 9, 10 and 11.

Example	Formulation	Flexural Strength	Flexural Modulus
6	2	11.4 (78.680 MPa)	5.4 (37,231.7 MPa)
6	3	9.2 (63.432 MPa)	3.6 (24,821.1 MPa)
9	4	12.6 (86.874 MPa)	4.3 (29,647.5 MPa)
9	4 (72-hr water boil)	7.3 (50.332 MPa)	4.2 (28,958.0 MPa)
10	5	9.1 (62.742 MPa)	3.0 (20,684.3 MPa)
11	2	12.4 (85.495 MPa)	4.2 (28,958.0 MPa)
		ksi	Msi

As can be seen, the panels made using the inorganic matrix composition in accordance with the present invention significantly outperformed (23% higher strength) the panel made without the acidic oxoanionic compound or the multivalent cationic compounds in the compositions in accordance with the present invention.

Example 7

Using the aqueous slurry composition of Example 2 and the process of Example 7, a composite was made from 30 plies of impregnated woven S-2 glass fabric. The composite was cured in a press at 180°C and 200 psi (or 1.378 MPa) pressure. After removing the material from the mold, the cured composite panel was post-baked at gradually increasing temperatures up to 400°C. The post-baked panel was machined into a disk, and inserted into cylinder to perform as an insulator within an aircraft braking system. The brake system was tested on a dynamometer to simulate an aborted takeoff, which placed extreme thermal shock on the entire system, including the insulator, which went from ambient temperature to 600°C within 3 seconds. The brake insulator made using the matrix material of the present invention passed without notable damage. The performance exceeded ceramic plates and organic composite materials, which were severely damaged during the test.

Example 8

The aqueous slurry composition of Example 2 was applied through squeeze rollers to a woven S-2 glass fabric. The impregnated fabric was placed between two layers of plastic film and rolled onto a tube. This roll of impregnated fabric was sealed and refrigerated to minimize drying. Approximately 24 hours later, a sheet of pre-impregnated fabric was removed from the roll, cut into a gasket shape, and placed between two pipe flanges which were subsequently bolted together to apply pressure to the impregnated fabric. The bolted joint was then gradually heated to cure the gasket. The reinforced matrix composition in accordance with the present invention functioned as a high-temperature insulating gasket. It was flexible during the initial mounting, effectively adapting to minor mismatches in the two flanges. If insulating washers are used, the two flanges are thermally isolated from each other. Further, the gasket could be made using non-woven fabrics and could be pre-cured rather than in situ cured, per the present example.

Example 9

The aqueous slurry composition of Examples 4 was used to impregnate, using a laboratory scale treater, an S-2 glass fabric 6781, which was taken from a 10 inch (25.4 cm) wide roll of fabric. The composition had a high viscosity, approximately that of honey, but it was useable and would impregnate the fabric. The roll was cut into sheets and staged at room temperature for 30 minutes. Ten sheets of fabric, which were similarly prepared, were layered on a release-coated surface to give a composite that was approximately 0.110 inch thick (0.2794 cm). The composite panel was then inserted into a vacuum bag and placed under vacuum of 28.5 inches of mercury (or 0.98138 Kgf/cm²) for 2 hours. The vacuum bagged panel was then inserted into a press between two plates and cured at 80°C for 3 hours under 200 psi (or 1.378 MPa) pressure and 28.5 inches of mercury (or 0.98138 Kgf/cm²) of vacuum. The panel was removed from the press and post baked at 80°C for 12 hours, 110°C for 12 hours, and 150°C for 4 hours. The panel was then demolded. One set of samples was tested in the as-molded condition. Another set of samples was placed in boiling water for 72 hours. The results are reported in Table 2. As can be seen from the results, strong panels can be made from alternative silica sources. The invention shows structural integrity after exposure to severe hot water conditions, even with a relatively low temperature cure.

Example 10

The aqueous slurry composition of Examples 5 was used to impregnate, using a laboratory scale treater, an S-2 glass fabric 6781, which was taken from a 10 inch (25.4 cm) wide roll of fabric. The composition had a viscosity of 1200 centipoise, and was effectively prepregged. The roll was cut into sheets and staged at room temperature for 30 minutes. Six sheets of fabric, which were similarly prepared, were layered on a release-coated surface. The composite panel was then inserted into a vacuum bag and placed under vacuum of 28.5 inches of mercury (or 0.98138 Kgf/cm²) for 2 hours. The vacuum bagged panel was then inserted into a press between two plates and cured at 80°C for 3 hours under 200 psi (or 1.378 MPa) pressure and 28.5 inches of mercury (or 0.98138 Kgf/cm²) of vacuum. The panel was removed from the press and post baked at 80°C for 12 hours, 110°C for 12 hours, and 150°C for 4 hours. The panel was then demolded and tested. The results are reported in Table 2. As can be seen from the results, strong panels can be made from alternative silica sources.

Example 11

The aqueous slurry composition of Examples 2 was used to impregnate, using a laboratory scale treater, an S-2 glass fabric 6781, which was taken from a 10 inch (25.4 cm) wide roll of fabric. The composition had a viscosity of 150 centipoise, and was effectively prepregged. The roll was cut into sheets and staged at room temperature for 30 minutes. Six sheets of fabric, which were similarly prepared, were layered on a release-coated surface. The composite panel was then inserted into a vacuum bag and placed under vacuum of 28.5 inches of mercury (or 0.98138 Kgf/cm²) for 2 hours. The vacuum bagged panel was then inserted into a press between two plates and cured at 80°C for 3 hours under 200 psi (or 1.378 MPa) pressure and 28.5 inches of mercury (or 0.98138 Kgf/cm²) of vacuum. The panel was then demolded and tested. The results are reported in Table 2. As can be seen from the results, alternative cure cycles are viable.

Example 12

Using the aqueous slurry composition of Example 2 and the process of Example 7, several composite panels were made from 4 plies of impregnated woven S-2 glass fabric. The composite was cured in a press at 180°C and 200 psi (or 1.378 MPa) pressure. The composite panels formed an adhesive bond to several materials placed within the mold. These materials

included steel, glass, plastic and PTFE. A cohesive failure mode was seen for both steel and glass when peeling the adhesive bond.

This technology may be applied to a wide variety of applications such as reinforced missile silo doors, ship decks, aircraft carrier blast and heat shields, fire barriers, hot gas filters, protective coatings, electrical panels and boxes (with and without EMI shielding), engine covers, or any application that would need, advantageously, protection from fire and heat transfer damage, corrosion resistance, lifecycle cost savings and weight reduction. Another example would be reinforced insulator inserts for aircraft brakes. The insulator within each piston thermally isolates the friction head from the hydraulic system. Compared to conventional resins, which decompose below 450°C, the matrix binders of the present invention have much higher thermal stability (to above 1000°C), and in contrast to metals, the composite of the present invention has superior insulation performance. This protects the hydraulic system and can reduce the weight and/or associated costs. In comparison to ceramics, the composite of the present invention is tougher because due to the presence of the reinforcing fibers, but less expensive than ceramic matrix composites due to the materials and processes utilized.

The foregoing embodiments of the present invention have been presented for the purposes of illustration and description. These descriptions and embodiments are not intended to be exhaustive or to limit the invention to the precise form disclosed, and obviously many modifications and variations are possible in light of the above disclosure. The embodiments were chosen and described in order to best explain the principle of the invention and its practical applications to thereby enable others skilled in the art to best utilize the invention in its various embodiments and with various modifications as are suited to the particular use contemplated. It is intended that the invention be defined by the following claims.

What we claim is:

1. A modified alkali silicate matrix composition comprising the reaction product of an alkali silicate and/or alkali silicate precursors, one or more acidic oxoanionic compounds, water
5 and optionally one or more compounds containing multivalent cation(s) selected from Groups 2, 3, 4, 5, 6, 11, 12, 13, 14, 15 or 16 of the periodic table and optionally a clay filler.

2. The composition of claim 1, wherein the alkali silicate is selected from potassium silicate solutions and/or sodium silicate solutions.

10 3. The composition of claim 1, wherein the alkali silicate is crystalline and/or amorphous sodium silicate and/or potassium silicate.

15 4. The composition of claim 1 wherein the alkali silicate precursors are an alkali base and a SiO_2 source.

20 5. The composition of claim 4 wherein the SiO_2 source is an amorphous or crystalline SiO_2 form, selected from the group consisting of silica, silica fume, microsilica, precipitated silica, sand, quartz, quartz flour, silica gels, fumed silica and colloidal silica.

6. The composition of claim 4 wherein the alkali base is an alkali hydroxide, alkali carbonate and/or an alkali oxide.

25 7. The composition of claim 6 wherein the alkali hydroxide is selected from the group consisting of potassium hydroxide and sodium hydroxide.

8. The composition of claim 1 wherein the alkali silicate and/or alkali silicate precursors has a $\text{SiO}_2/\text{A}_2\text{O}$ ratio of 2.0:1.0 to 20.0:1.0, where A is K (potassium) and/or Na (sodium).

30 9. The composition of claim 1, wherein said acidic oxoanionic compound is selected from the group of consisting of boric acid, phosphoric acid, sulfuric acid, nitric acid, sodium dihydrogen phosphate, disodium hydrogen phosphate, their potassium analogs, their ammonium analogs, and mixtures thereof.

10. The composition of claim 1, wherein the acidic oxoanionic compound is phosphoric acid.

11. The composition of claim 1, wherein the compounds containing multivalent cation(s) are selected from the group compounds incorporating boron, aluminum, lead, zinc, gallium, cadmium, titanium, zirconium, lanthanum, cerium, neodymium, yttrium, calcium, magnesium, strontium and barium.

12. The composition of claim 1, wherein the compounds containing multivalent cation(s) are selected from the group consisting of magnesium nitrate, magnesium sulfate and magnesium chloride.

13. The composition of claim 1 wherein the compounds containing multivalent cation(s) is magnesium nitrate.

14. The composition of claim 1 wherein the clay filler is kaolin, calcined kaolin, mica and/or metakaolin.

15. The composition of claim 1, wherein said alkali silicate and/or alkali silicate precursors are present in an amount between 30 wt. % and 90 wt. % based upon the total composition.

16. The composition of claim 1, wherein said alkali silicate is formed from a alkali hydroxide and a SiO_2 source and said alkali hydroxide is present in an amount of between 3 wt. % to 25 wt. % and said SiO_2 source is present in an amount of 15 wt. % to 75 wt. % based upon the total composition weight.

17. The composition of claim 1, wherein said acidic oxoanionic compound is present in an amount of between 0.01 wt. % and 20 wt. % based upon the total composition.

18. The composition of claim 1, wherein said compounds containing multivalent cation(s) is present in an amount of between zero and 20 wt. % based upon the total composition.

19. The composition of claim 1, wherein said clay filler is present in an amount of between 0.0 wt. % and 25 wt. % based upon the total composition weight.

20. The composition of claim 1 wherein the network comprises the reaction product of the following:

- a) 30 to 90 wt. % of alkali silicate,
- b) 0.01 to 20 wt. % of phosphoric acid,
- c) 0 to 25 wt. % of a clay filler,
- d) 0 to 20 wt. % of alkaline earth salt and
- e) 10 to 70 wt. % of water.

21. The composition of claim 1, wherein the network comprises the reaction product of the following:

- a) 10 to 75 wt. % of a SiO_2 source,
- b) 3 to 25 wt. % of an alkali hydroxide,
- c) 0.01 to 20 wt. % of phosphoric acid,
- d) 0 to 25 wt. % of a clay filler,
- e) 0 to 20 wt. % of alkaline earth salt and
- f) 10 to 70 wt. % of water.

22. The composition of claim 1 wherein the network comprises the reaction product of the following (excluding water):

- a) 30 to 90 wt. % of alkali silicate,
- b) 0.01 to 30 wt. % of phosphoric acid,
- c) 0 to 30 wt. % of a clay filler and
- d) 0 to 25 wt. % of alkaline earth salt.

23. The composition of claim 1 wherein the network comprises the reaction product of the following (excluding water):

- a) 10 to 90 wt. % of SiO_2 source,
- b) 3 to 25 wt. % of alkali hydroxide,
- c) 0.01 to 30 wt. % of phosphoric acid,
- d) 0 to 30 wt. % of a clay filler and

e) 0 to 25 wt. % of alkaline earth salt.

24. The composition of claim 1, wherein the network also includes non-clay filler materials.

5 25. The composition of claim 24, wherein the filler materials are selected from the group consisting of fibers, spheres, and particles.

26. The composition of claim 25, wherein the fibers are selected from a group consisting of continuous fibers and discontinuous fibers.

10

27. The composition of claim 25, wherein the spheres are selected from the group consisting of microspheres, macrospheres, hollow spheres, and solid spheres comprising glass, ceramic, metal, mineral, organic or inorganic materials.

15 28. The composition of claim 25, wherein the filler materials are utilized for reinforcement and selected from the group consisting of carbon fibers, glass fibers, alkali resistant glass fibers, organic fibers, ceramic fibers, mineral fibers and metallic fibers.

20 29. The composition of claim 28, wherein the reinforcement materials are selected from the group consisting of graphite fibers, E-glass fibers, S-glass fibers, basalt fibers, stainless steel fibers, titanium fibers, nickel alloy fibers, aramid fibers, polyethylene fibers, SiC fibers and BN fibers.

30 30. The inorganic matrix composition of claim 1 formed by curing the composition at a temperature ranging from 15°C to 1000°C+, an external pressure from ambient to 20,000 psi (137.895 MPa), and optionally under a vacuum of from ambient to 10^{-3} torr.

31. The inorganic matrix composition of claim 1 formed by curing the composition at 15°C to 200°C and an external pressure from ambient to 200 psi (or 1.378 MPa), and optionally
30 under a vacuum of from ambient to 10^{-3} torr.

32. A method of making an inorganic silicate composite comprising the steps of

applying an aqueous slurry of a mixture of an alkali silicate, phosphoric acid, a clay filler, an alkaline earth salt and water to a reinforcing medium and curing the composite by applying heat at a temperature of 15°C up to 1000°C+, an external pressure from ambient to 20,000 psi (137.895 MPa) and under, and optionally under a vacuum of ambient to 10^{-3} torr.

5

33. The method of claim 32 wherein the composite is cured preferably at a temperature of 15°C up to 200°C and an external pressure from ambient to 200 psi (or 1.378 MPa), and optionally under a vacuum of ambient to 10^{-3} torr.

10

34. The method of claim 32 wherein the uncured composite is in form of bulk molding compound, sheet molding compound, powder and reinforcement, liquid and reinforcement or prepreg.

15

35. The method of claim 32 wherein the composite is cured using processes which include compression molding, pultrusion, wet lay-up, filament winding, autoclave vacuum bag processing, non-autoclave vacuum bag processing, vacuum infusion, liquid resin, film infusion or powder infusion, resin transfer molding, extrusion, injection molding, casting, spin casting, trapped elastomer molding and like processes.

20

36. The method of claim 32 wherein the composite is consolidated before and/or during the curing process.

25

37. The method of claim 32 wherein the slurry includes additional filler materials selected from the group consisting of carbon fibers, glass fibers, alkali resistant fibers, mineral fibers, organic fibers, ceramic fibers and metallic fibers.

30

38. The method of claim 32 wherein the slurry includes additional filler materials selected from the group consisting of graphite fibers, E-glass fibers, S-glass fibers, stainless steel fibers, titanium fibers, nickel alloy fibers, aramid fibers, polyethylene fibers, basalt fibers, SiC fibers and BN fibers.

39. The method of claim 32 wherein the reinforcing medium is a glass fiber such as an E-glass fiber, S-glass fiber and/or an alkaline resistant fiber.

40. An alkali silicate slurry composition for forming an inorganic polymer network comprising an alkali silicate or a mixture that yields an insitu alkali silicate, an acidic oxoanionic compound, water and optionally one or more compounds containing multivalent cation(s) selected from Groups 2, 3, 4, 5, 6, 11, 12, 13, 14, 15 or 16 of the periodic table and optionally a modifier that moderates the gelation of matrix binder suspension and/or optionally a clay filler to enhance physical and thermal properties.

41. The composition of claim 40, wherein the gel modifier is an organic acid or organic base.

42. The composition of claim 41, wherein said organic acid is an α -hydroxyacid and/or a β -hydroxyacid.

43. The composition of claim 41, wherein said organic base is substituted nitrogen organic base.

44. The composition of claim 41, wherein said organic base is a substituted pyridine.

45. The composition of claim 41, wherein said organic base is quinoline.

46. The composition of claim 40, wherein said gel modifier is present in an amount of between zero and 10 wt. % based upon the total composition.

47. A method of making an inorganic silicate composite comprising the steps of applying an aqueous slurry of a mixture of an alkali silicate, phosphoric acid, water and optionally a clay filler, an alkaline earth salt and/or a gel modifier to a reinforcing medium and curing the composite by applying heat at a temperature of 15°C up to 1000°C and external pressures from ambient pressure to 20,000 psi (137.895 MPa) and/or under a vacuum of from ambient to 10^{-3} torr.

(19) World Intellectual Property Organization
International Bureau



(43) International Publication Date
28 March 2002 (28.03.2002)

PCT

(10) International Publication Number
WO 02/24597 A3

(51) International Patent Classification⁷: C04B 28/26

(21) International Application Number: PCT/US01/29376

(22) International Filing Date:
18 September 2001 (18.09.2001)

(25) Filing Language: English

(26) Publication Language: English

(30) Priority Data:
60/233,952 20 September 2000 (20.09.2000) US
09/871,765 1 June 2001 (01.06.2001) US

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(81) Designated States (*national*): AE, AG, AL, AM, AT, AU,
AZ, BA, BB, BG, BR, BY, BZ, CA, CH, CN, CO, CR, CU,
CZ, DE, DK, DM, DZ, EC, EE, ES, FI, GB, GD, GE, GH,
GM, HR, HU, ID, IL, IN, IS, JP, KE, KG, KP, KR, KZ, LC,
LK, LR, LS, LT, LU, LV, MA, MD, MG, MK, MN, MW,
MX, MZ, NO, NZ, PH, PL, PT, RO, RU, SD, SE, SG, SI,
SK, SL, TJ, TM, TR, TT, TZ, UA, UG, UZ, VN, YU, ZA,
ZW.

(84) Designated States (*regional*): ARIPO patent (GH, GM,
KE, LS, MW, MZ, SD, SL, SZ, TZ, UG, ZW), Eurasian
patent (AM, AZ, BY, KG, KZ, MD, RU, TJ, TM), European
patent (AT, BE, CH, CY, DE, DK, ES, FI, FR, GB, GR, IE,
IT, LU, MC, NL, PT, SE, TR), OAPI patent (BF, BJ, CF,
CG, CI, CM, GA, GN, GQ, GW, ML, MR, NE, SN, TD,
TG).

Published:

- with international search report
- before the expiration of the time limit for amending the
claims and to be republished in the event of receipt of
amendments

(88) Date of publication of the international search report:
13 June 2002

For two-letter codes and other abbreviations, refer to the "Guid-
ance Notes on Codes and Abbreviations" appearing at the begin-
ning of each regular issue of the PCT Gazette.

(54) Title: INORGANIC MATRIX COMPOSITIONS, COMPOSITES AND PROCESS OF MAKING THE SAME

(57) Abstract: A modified alkali silicate composition for forming an inorganic network is made by reacting an alkali silicate (or precursors such as an alkali hydroxide, a SiO₂ source and water), an acidic oxoanionic compound such as phosphoric acid, water and optionally one or more multivalent cation(s) selected from Groups 2, 3, 4, 5, 6, 11, 12, 13, 14, 15 or 16 of the periodic table such as an alkaline earth salt, water and optional processing aids. A composite can be prepared by applying the modified aqueous alkali silicate composition to a reinforcing medium and curing the composite at a temperature from 15°C up to 1000°C and a pressure of up to 20,000 psi (137.895 MPa). Composite and neat resin components prepared from the invention can exhibit excellent dimensional stability to 1000°C and higher, and can be prepared at temperatures and pressures typical for organic polymer processing. The composite can be shaped by compression molding as well as other known fabrication methods.

WO 02/24597 A3

INTERNATIONAL SEARCH REPORT

International Application No

PC/US 01/29376

A. CLASSIFICATION OF SUBJECT MATTER
IPC 7 C04B28/26

According to International Patent Classification (IPC) or to both national classification and IPC

B. FIELDS SEARCHED

Minimum documentation searched (classification system followed by classification symbols)
IPC 7 C04B

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Electronic data base consulted during the international search (name of data base and, where practical, search terms used)

EPO-Internal

C. DOCUMENTS CONSIDERED TO BE RELEVANT

Category *	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
X	CHEMICAL ABSTRACTS, vol. 85, no. 8, 23 August 1976 (1976-08-23) Columbus, Ohio, US; abstract no. 51069s, M.TANAKA: "Nonflammable inorganic foam" XP000063264 abstract & JP 51 034923 A (TANAKA) 25 March 1976 (1976-03-25) --- -/-	1-3,8,9, 11,17, 18,24, 25,28, 30,32

☒ Further documents are listed in the continuation of box C.

☒ Patent family members are listed in annex.

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- *8* document member of the same patent family

Date of the actual completion of the international search

28 March 2002

Date of mailing of the international search report

08/04/2002

Name and mailing address of the ISA

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Authorized officer

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INTERNATIONAL SEARCH REPORT

International Application No.

PCT/US 01/29376

C.(Continuation) DOCUMENTS CONSIDERED TO BE RELEVANT

Category *	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
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